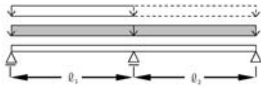


Structural analysis

TWO-SPAN BEAM - VIBRATION

04/2012



Two-span beam_Vibration

In accordance with approval Z 9.1-559
DIN 1052 (2008) and/or EN 1995-1-1 (2006)

Dead weight gk*)	Imposed load nk	Span of single-span beam											
		3,00 m	3,50 m	4,00 m	4,50 m	5,00 m	5,50 m	6,00 m	6,50 m	7,00 m			
1,00	1,00	60 L3s	80 L3s	80 L3s	100 L3s	120 L3s	140 L5s	160 L5s – 2	180 L5s	220 L7s – 2			
	2,00	80 L3s	90 L3s	90 L3s	120 L3s	120 L3s	200 L5s						
	2,80	80 L3s	80 L3s	100 L3s	120 L3s	140 L5s	180 L5s						
	3,50		90 L3s				200 L5s						
	4,00		100 L3s				220 L7s – 2						
5,00	120 L3s	240 L7s – 2											
1,50	1,00	80 L3s	80 L3s	90 L3s	120 L3s	140 L5s	160 L5s – 2	180 L5s	220 L7s – 2	220 L7s – 2			
	2,00	80 L3s		100 L3s	120 L3s	140 L5s	160 L5s – 2	200 L5s					
	2,80			100 L3s									
	3,50			90 L3s				180 L5s					
	4,00			100 L3s				220 L7s – 2					
5,00	120 L3s	140 L5s	160 L5s – 2	180 L5s	220 L7s – 2	240 L7s – 2							
2,00	1,00	80 L3s	80 L3s	100 L3s	120 L3s	140 L5s	160 L5s – 2	200 L5s	220 L7s – 2	240 L7s – 2			
	2,00		80 L3s	120 L3s	140 L5s	160 L5s – 2	180 L5s	220 L7s – 2					
	2,80			90 L3s									
	3,50			100 L3s							200 L5s		
	4,00			120 L3s							240 L7s – 2		
5,00	140 L5s	160 L5s – 2	180 L5s	220 L7s – 2	260 L7s – 2								
2,50	1,00	80 L3s	80 L3s	120 L3s	140 L5s	160 L5s – 2	180 L5s	220 L7s – 2	240 L7s – 2	260 L7s – 2			
	2,00		90 L3s	120 L3s			200 L5s						
	2,80		90 L3s										
	3,50		100 L3s										
	4,00		120 L3s										
5,00	140 L5s	160 L5s – 2	180 L5s	220 L7s – 2	240 L7s – 2	260 L7s – 2							
3,00	1,00	80 L3s	90 L3s	120 L3s	140 L5s	160 L5s – 2	200 L5s	220 L7s – 2	240 L7s – 2	240 L7s – 2			
	2,00		90 L3s										
	2,80		100 L3s							160 L5s – 2	200 L5s	220 L7s – 2	240 L7s – 2
	3,50												
	4,00												
5,00	160 L5s – 2	220 L7s – 2	280 L7s – 2										

* The CLT self-weight is already taken into account in the table at $\rho = 500 \text{ kg/m}^3$

Service class 1, imposed load category A ($\psi_0 = 0.7$; $\psi_1 = 0.5$; $\psi_2 = 0.3$)

Load-bearing capacity:

- Verification of bending stresses
- Verification of shearing stresses

$k_{mod} = 0.8$

Serviceability:

- Quasi-constant design situation
 $zul w_{fin} = 250$
- Infrequent design situation:
 $zul w_{q,inst} = 300$
 $zul w_{fin} - w_{g,inst} = 200$
- Vibration
Vibration according to EN 1995-1-1 and Kreuzinger & Mohr
($f_1 > 8 \text{ Hz}$ or $f_1 > 5 \text{ Hz}$ with $a = 0.4 \text{ m/s}^2$, $v < v_{grenz}$, $w_{ef} < 1 \text{ mm}$)
 $D = 2\%$, 5 cm cement screed, $b = 1.2 \cdot \ell$
 $k_{def} = 0.6$

Fire resistance

$\beta = 0.65 \text{ mm/min}$

R0
R30
R60
R90

Since any vibration depends not only on the span but also on the mass, a thicker ceiling may be necessary despite a shorter span. The analysis was carried out using the imposed load on one field. In the event of imposed loads on both fields, the required ceiling thickness may be reduced.

This table specifies the required thicknesses for the normal design situation (R0). The colour shading represents the fire resistance time which is also attained with this thickness. If a higher fire resistance time is required, a separate analysis must be carried out.

This table is only for preliminary estimate purposes and is not a substitute for a structural analysis.